

Chapter 4

Discrete Systems

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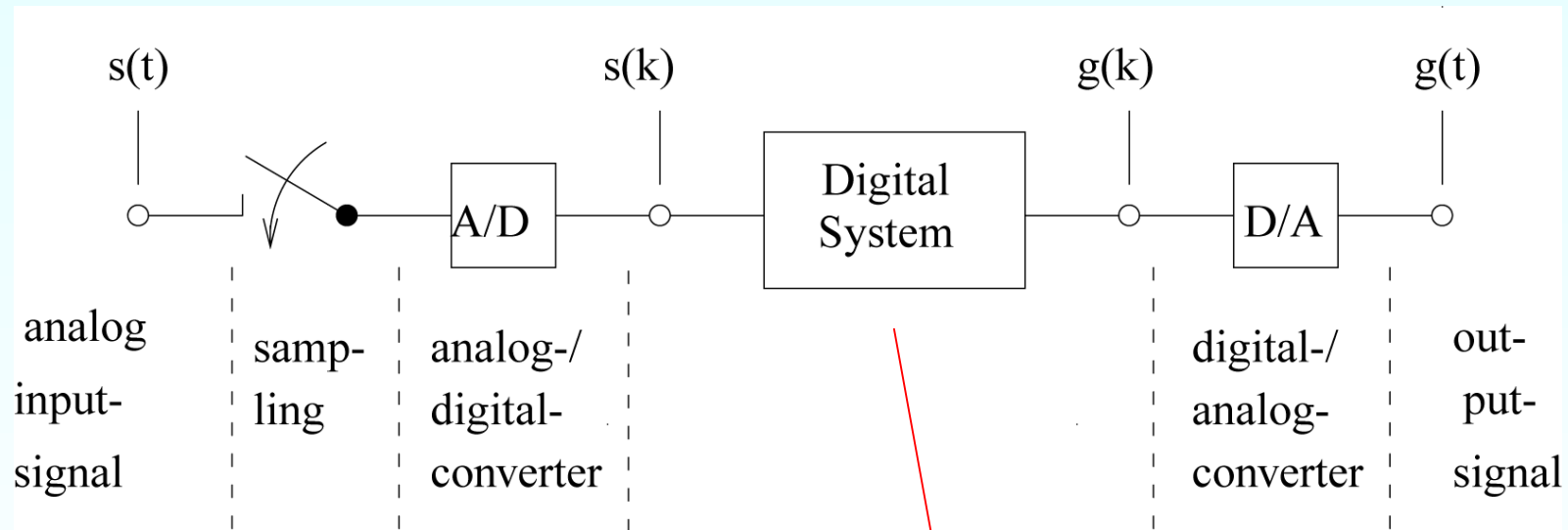
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4.1 Introduction

Graphik shows general scheme of a digital signal processing system (used in sound cards, digital sound processors, precise filtering applications etc.).

Note: In general additional low-pass filters are needed!

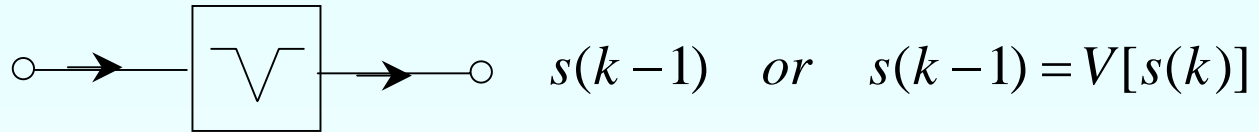


$$\{s(k)\} \rightarrow \{g(k)\} = T[\{s(k)\}] \quad \text{where } k = -\infty \dots +\infty$$

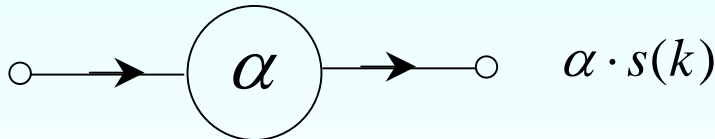
4.1 Introduction

In practice, such a system is represented by a digital signal processor, essentially consisting of the following elements:

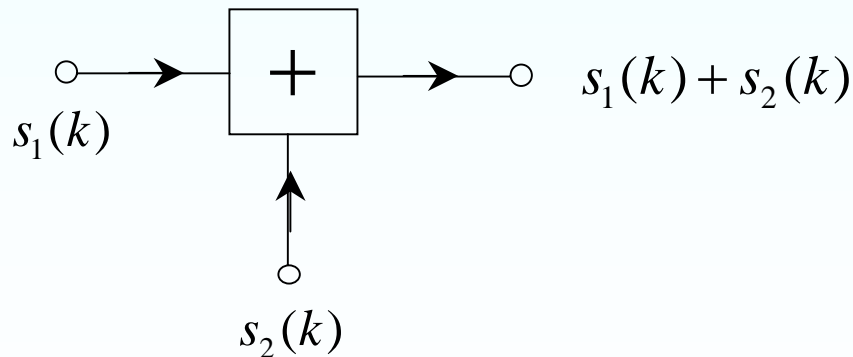
Delay:



Multipliier:



Adder:



4.1 Introduction

Example:

The relation of the example from section 2.3.5.1 with

$$g(k+2) + c_1 g(k+1) + g(k) = s(k+1) + s(k)$$

can be rewritten as:

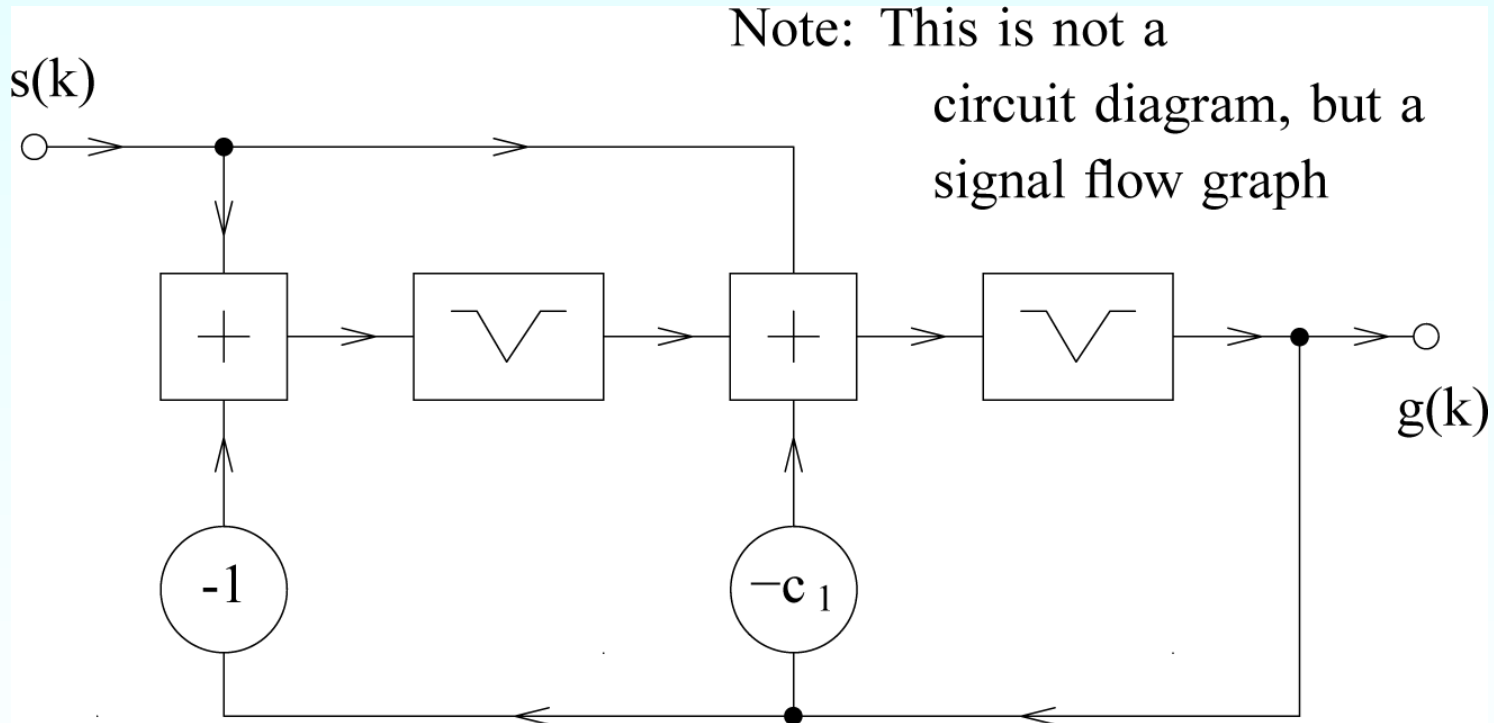
$$g(k+2) = -c_1 g(k+1) - g(k) + s(k+1) + s(k)$$

$$g(k) = -c_1 g(k-1) - g(k-2) + s(k-1) + s(k-2)$$

The corresponding signal flow is represented in the following diagram:



4.1 Introduction



Signal flow diagram of the example of a digital filter

4.1 Introduction

The same basic properties as for analog filters can also be found for discrete systems:

1- Real values:

From real-valued $\{s(k)\}$ follows that also $\{g(k)\}$ is real-valued

2- Time-invariance:

$$\{s(k)\} \rightarrow \{g(k)\} \quad \text{gives} \quad \{s(k + \kappa)\} \rightarrow \{g(k + \kappa)\}$$

3- Linearity:

$$\begin{array}{l} \{s_1(k)\} \rightarrow \{g_1(k)\} \\ \{s_v(k)\} \rightarrow \{g_v(k)\} \\ \{s_n(k)\} \rightarrow \{g_n(k)\} \end{array} \quad \Rightarrow \quad \sum_{v=1}^n \{\alpha_v s_v(k)\} \rightarrow \sum_{v=1}^n \{\alpha_v g_v(k)\}$$

Causality and stability are here as important as for analog systems.



4.2 Linear, Time-Invariant Discrete Systems

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4.2.1 Difference Equations

The most important class of discrete LTI-systems is the one, describable by an n-th order equation of the following kind:

$$\sum_{\alpha=0}^n a_{\alpha} s(k - \alpha) = \sum_{\beta=0}^n b_{\beta} g(k - \beta)$$

From this, one obtains:

$$g(k) = \frac{1}{b_0} \left[\sum_{\alpha=0}^n a_{\alpha} s(k - \alpha) - \sum_{\beta=1}^n b_{\beta} g(k - \beta) \right]$$



4.2.1 Difference Equations

Definition:

A discrete-time LTI-system is called recursive if the calculation of each output value $g(k)$ from the preceding output values $g(k - \beta)$ with $\beta > 0$ is performed.

Definition:

A causal digital LTI-system is called non-recursive if the calculation of each output value $g(k)$ is possible without the use of previously calculated output signals $g(k - \beta)$ with $\beta > 0$.



4.2.1 Difference Equations

Example:

Given is a second order discrete LTI-system, where $n = m = 2$, thus:

$$g(k) = \frac{1}{b_0} \left[\sum_{\alpha=0}^2 a_{\alpha} s(k - \alpha) - \sum_{\beta=1}^2 b_{\beta} g(k - \beta) \right]$$

One can set $b_0 = 1$ here without any restrictions:

$$g(k) = a_0 s(k) + a_1 s(k - 1) + a_2 s(k - 2) - b_1 g(k - 1) - b_2 g(k - 2)$$

In the next slide it is specified: $b_{1,2} = d_{1,2} !!$



4.2.1 Difference Equations

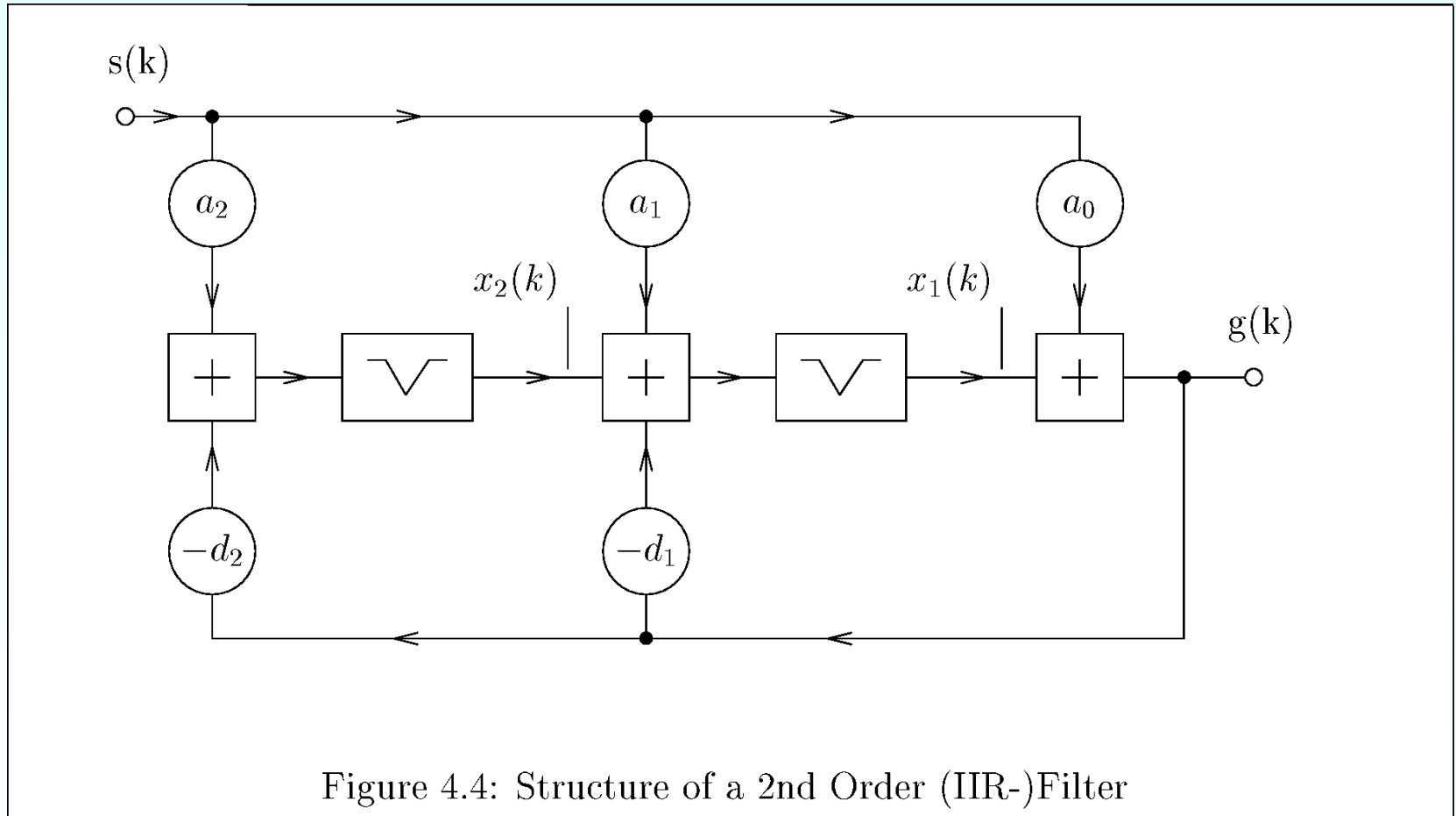


Figure 4.4: Structure of a 2nd Order (IIR-)Filter

4.2.2 The Discrete Impulse Response

Definition:

The impulse response of a discrete system is the response $g(k)$ of the system to $s(k) = \gamma_0(k)$

This special sequence to be observed at the output is denoted by: $h(k)$

The answer of the system to any causal excitation $s(k)$ with $s(k) \equiv 0$ for $k < 0$ thus is:

$$g(k) = \sum_{\nu=0}^{+\infty} h(\nu) \cdot s(k - \nu) = h(k) * s(k) \quad \longrightarrow \quad \text{Discrete convolution}$$

The causality provides: $h(k) \equiv 0$ for $k < 0$, thus

$$s(k) = g(k) \equiv 0 \quad \text{for} \quad k < 0$$



4.2.3 The Discrete Transfer Function $H_z(z)$

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4.2.3 The Discrete Transfer Function $H_z(z)$

If $\{s(k)\}$ as input signal for a discrete system is used with

$$s(k) = Ue^{kpT} = Uz^k \quad \text{where } k = 0 \dots \infty$$

and with $p = \sigma + j\omega$ being the complex frequency, one gets:

$$\begin{aligned} g(k) &= h(k) * s(k) = \sum_{v=0}^{+\infty} h(v) \cdot s(k-v) \\ &= \sum_{v=0}^{+\infty} h(v) \cdot Uz^{k-v} = Uz^k \underbrace{\sum_{v=0}^{+\infty} h(v) \cdot z^{-v}}_{Z\{h(v)\}=H_z(z)} = Uz^k \cdot H_z(z) \end{aligned}$$

Discrete transfer function.



4.2.3 The Discrete Transfer Function $H_z(z)$

* According to z-transform properties it holds:

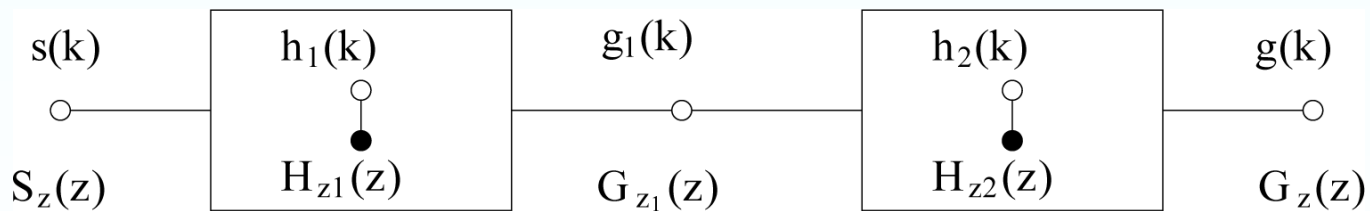
$$g(k) = \sum_{v=0}^{+\infty} h(v) \cdot s(k-v) = h(k) * s(k) \quad \circ \text{---} \bullet \quad G_z(z) = H_z(z) \cdot S_z(z)$$

$$\Leftrightarrow H_z(z) = \frac{G_z(z)}{S_z(z)}$$

* The discrete transfer function is the z-transform of the impulse response $\{h(k)\}$

$$H_z(z) = \sum_{v=0}^{+\infty} h(v) \cdot z^{-v}$$

* For a chain of two discrete LTI-systems it holds:



4.2.3 The Discrete Transfer Function $H_z(z)$

With the equations:

$$g_1(k) = h_1(k) * s(k) \quad \text{and} \quad g(k) = g_1(k) * h_2(k)$$

it follows: $g(k) = g_1(k) * h_2(k) = [h_1(k) * s(k)] * h_2(k)$

or $g(k) = h_1(k) * h_2(k) * s(k)$ $\circ \rightarrow \bullet$ $G_z(z) = \underbrace{H_{z1}(z) \cdot H_{z2}(z)}_{H_z(z)} \cdot S_z(z)$

$$G_z(z) = H_z(z) \cdot S_z(z) \quad \leftarrow H_z(z) = H_{z1}(z)H_{z2}(z)$$



4.2.3 The Discrete Transfer Function $H_z(z)$

Considering a difference equation, this relation can be described in the z-domain:

$$\sum_{\alpha=0}^n a_{\alpha} s(k - \alpha) = \sum_{\beta=0}^n b_{\beta} g(k - \beta)$$

The z-transform of both sides of the equation is then:

$$\sum_{\alpha=0}^n a_{\alpha} S_z(z) \cdot z^{-\alpha} = \sum_{\beta=0}^n b_{\beta} G_z(z) \cdot z^{-\beta}$$

Rewriting this formula gives:

$$H_z(z) = \frac{G_z(z)}{S_z(z)} = \frac{\sum_{\alpha=0}^n a_{\alpha} \cdot z^{-\alpha}}{\sum_{\beta=0}^n b_{\beta} \cdot z^{-\beta}} \xrightarrow{\text{By means of an index conversion}} H_z(z) = \frac{\sum_{\mu=0}^m d_{\mu} \cdot z^{\mu}}{\sum_{\nu=0}^n c_{\nu} \cdot z^{\nu}} \quad \text{where } n \geq m$$



4.2.3 The Discrete Transfer Function $H_z(z)$

So this second form of the discrete transfer function $H_z(z)$ is a rational function of the variable z :

$$H_z(z) = \frac{\text{Numerator polynom in } z}{\text{Denominator ploynom in } z} = \frac{P(z)}{Q(z)}$$

A third form of the discrete transfer function is based on the zeros of the numerator and the denominator polynom:

$$H_z(z) = \frac{d_m}{c_n} \cdot \frac{\prod_{\mu=1}^m (z - z_{0\mu})}{\prod_{\nu=1}^n (z - z_{\infty\nu})}$$

Roots of the of the numerator or the zeros

Roots of the denominator or the poles



4.2.4 General Properties of $H_z(z)$

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4.2.4 General Properties of $H_z(z)$

1. Properties of system coefficients and of poles and zeros:

→ The coefficients respectively are real constants. The zeros and poles are either real or conjugated complex:

$$z_{0_{\mu_1}} = |z_{0_{\mu_1}}| e^{j\psi_{0_{\mu_1}}} \quad \text{where } z_{0_{\mu_2}} = z_{0_{\mu_1}}^* = |z_{0_{\mu_1}}| e^{-j\psi_{0_{\mu_1}}}$$

$$z_{\infty_{v_1}} = |z_{\infty_{v_1}}| e^{j\psi_{\infty_{v_1}}} \quad \text{where } z_{\infty_{v_2}} = z_{\infty_{v_1}}^* = |z_{\infty_{v_1}}| e^{-j\psi_{\infty_{v_1}}}$$

2. Stability: (BIBO: bounded input bounded output criterion)

A discrete system obviously is stable, if

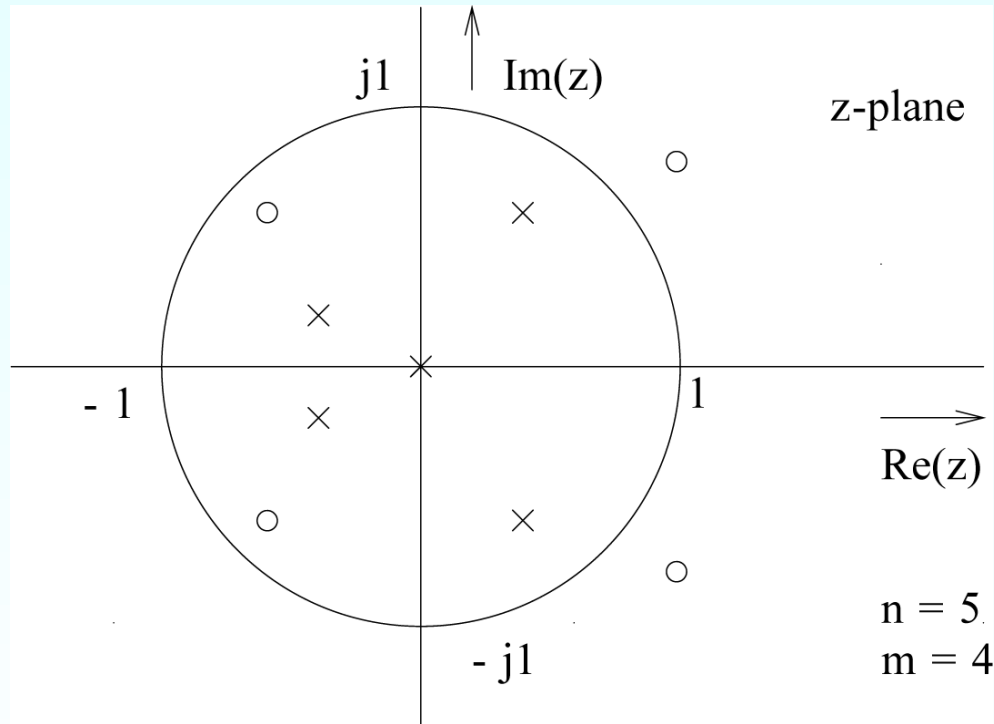
any bounded input signal $|s(k)| < M_1 < \infty \quad \forall k$ causes

a bounded output signal $|g(k)| < M_2 < \infty$



4.2.4 General Properties of $H_z(z)$

BIBO stability is given, if the following relation holds: $|z_{\infty v}| < 1 \quad \forall v$



Pole- zero plot of a real, causal and stable system

4.2.5 Behaviour of $H_z(z)$ on the unit circle

If we observe the $H_z(z)$ for any point z on the unit circle with $|z| = 1$ and $z = e^{j\omega T}$ we obtain the so-called frequency response.

$$H_z(e^{j\omega T}) = \frac{\sum_{\alpha=0}^n a_{\alpha} e^{-j\alpha\omega T}}{\sum_{\beta=0}^n b_{\beta} e^{-j\beta\omega T}} = \frac{d_m \prod_{\mu=1}^m (e^{j\omega T} - z_{0_{\mu}})}{c_n \prod_{\nu=1}^n (e^{j\omega T} - z_{\infty_{\nu}})}$$

→ periodic function with $\omega T = 2\pi$ or $\omega = \frac{2\pi}{T}$

In short: $H_z(e^{j\omega T}) = H_a(\omega)$



4.2.5 Behaviour of $H_z(z)$ on the unit circle

In general :

$$G_z(z) = H_z(z)S_z(z) \Rightarrow G_z(e^{j\omega T}) = H_z(e^{j\omega T})S_z(e^{j\omega T})$$

A normalized representation using $\omega T = \Omega$ or $F = \Omega \cdot 2\pi$, leads to:

$$H_z(e^{j\omega T}) = H_z(e^{j\Omega}) = H_{Na}(\Omega) = \frac{b_m \prod_{\mu=1}^m (e^{j\Omega} - z_{0\mu})}{c_n \prod_{\nu=1}^n (e^{j\Omega} - z_{\infty\nu})}$$

Magnitude $|H_a(\Omega)|$ and its phase $\varphi_a(\Omega)$ can be rewritten as:

$$H_{Na}(\Omega) = |H_{Na}(\Omega)| e^{j\varphi_{Na}(\Omega)}$$



4.2.5 Behaviour of $H_z(z)$ on the unit circle

For the distance of each zero or each pole to the unit circle, it holds:

$$\begin{aligned} |e^{j\Omega} - z| &= |\cos \Omega + j \sin \Omega - |z| \cos \psi - |z| \cdot j \sin \psi| \\ &= \sqrt{(\cos \Omega - |z| \cos \psi)^2 + (\sin \Omega - |z| \sin \psi)^2} \\ &= \sqrt{\cos^2 \Omega - 2 \cos \Omega |z| \cos \psi + |z|^2 \cos^2 \psi + \sin^2 \Omega - 2 \sin \Omega |z| \sin \psi + |z|^2 \sin^2 \psi} \\ &= \sqrt{1 - 2|z| \cos(\Omega - \psi) + |z|^2} \end{aligned}$$

with $z = |z| e^{j\psi}$

For the corresponding angle of the connection of each zero or each pole to the unit circle, it holds:

$$\angle (e^{j\Omega} - z) = \arctan \frac{\sin \Omega - |z| \sin \psi}{\cos \Omega - |z| \cos \psi}$$



4.2.5 Behaviour of $H_z(z)$ on the unit circle

Thus it results:

$$\begin{aligned}
 |H_{Na}(\Omega)| &= \left| \frac{b_m}{c_n} \right| \cdot \frac{\prod_{\mu=1}^m |e^{j\Omega} - z_{0\mu}|}{\prod_{\nu=1}^n |e^{j\Omega} - z_{\infty\nu}|} \\
 &= \left| \frac{b_m}{c_n} \right| \cdot \frac{\prod_{\mu=1}^m \sqrt{1 - 2|z_{0\mu}| \cdot \cos(\Omega - \psi_{0\mu}) + |z_{0\mu}|^2}}{\prod_{\nu=1}^n \sqrt{1 - 2|z_{\infty\nu}| \cdot \cos(\Omega - \psi_{\infty\nu}) + |z_{\infty\nu}|^2}}
 \end{aligned}$$

With $\frac{b_m}{c_n} > 0$ it follows:

$$\varphi_{Na}(\Omega) = \sum_{\nu=1}^n \arctan \frac{\sin \Omega - |z_{\infty\nu}| \sin \Psi_{\infty\nu}}{\cos \Omega - |z_{\infty\nu}| \cos \Psi_{\infty\nu}} - \sum_{\mu=1}^m \arctan \frac{\sin \Omega - |z_{0\mu}| \sin \Psi_{0\mu}}{\cos \Omega - |z_{0\mu}| \cos \Psi_{0\mu}}$$



4.2.5 Behaviour of $H_z(z)$ on the unit circle

For the derivative of the angle related to the connections of each pole or each zero it holds:

$$\begin{aligned}
 \frac{d}{d\Omega}(e^{j\Omega} - z) &= \frac{d}{d\Omega} \arctan \frac{\sin \Omega - |z| \sin \psi}{\cos \Omega - |z| \cos \psi} = \\
 &= \frac{1}{1 + \frac{(\sin \Omega - |z| \sin \psi)^2}{(\cos \Omega - |z| \cos \psi)^2}} \cdot \frac{\cos \Omega (\cos \Omega - |z| \cos \psi) - (-\sin \Omega) (\sin \Omega - |z| \sin \psi)}{(\cos \Omega - |z| \cos \psi)^2} \\
 &= \frac{\cos^2 \Omega - \cos \Omega |z| \cos \psi + \sin^2 \Omega - \sin \Omega |z| \sin \psi}{(\cos \Omega - |z| \cos \psi)^2 + (\sin \Omega - |z| \sin \psi)^2} \\
 &= \frac{1 - |z| \cos(\Omega - \psi)}{\cos^2 \Omega - 2 \cos \Omega |z| \cos \psi + |z|^2 \cos^2 \psi + \sin^2 \Omega - 2 \sin \Omega |z| \sin \psi + |z|^2 \sin^2 \psi} \\
 &= \frac{1 - |z| \cos(\Omega - \psi)}{1 + |z|^2 - 2 |z| \cos(\Omega - \psi)}
 \end{aligned}$$



4.2.5 Behaviour of $H_z(z)$ on the unit circle

Thus the frequency normalised envelope delay results to:

$$\tau_{Nga}(\Omega) = \frac{d\varphi_{Na}(\Omega)}{d\Omega} = \sum_{v=1}^n \frac{1 - |z_{\infty v}| \cdot \cos(\Omega - \Psi_{\infty v})}{1 - 2|z_{\infty v}| \cdot \cos(\Omega - \Psi_{\infty v}) + |z_{\infty v}|^2} - \sum_{\mu=1}^m \frac{1 - |z_{0\mu}| \cdot \cos(\Omega - \Psi_{0\mu})}{1 - 2|z_{0\mu}| \cdot \cos(\Omega - \Psi_{0\mu}) + |z_{0\mu}|^2}$$

Note: According to the formulas given above it follows:

$$|H_{Na}(\Omega)| = |H_{Na}(-\Omega)| \quad \varphi_{Na}(-\Omega) = -\varphi_{Na}(\Omega)$$

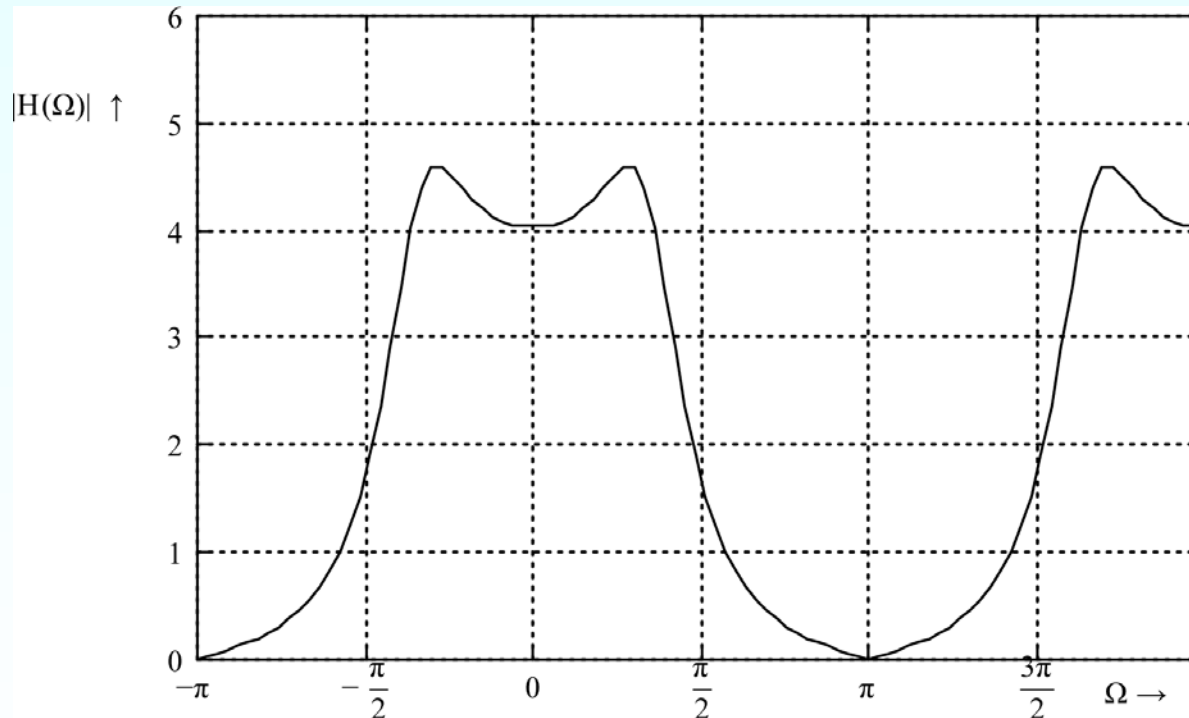
$$\tau_{Nga}(-\Omega) = \tau_{Nga}(\Omega)$$



4.2.5 Behaviour of $H_z(z)$ on the unit circle

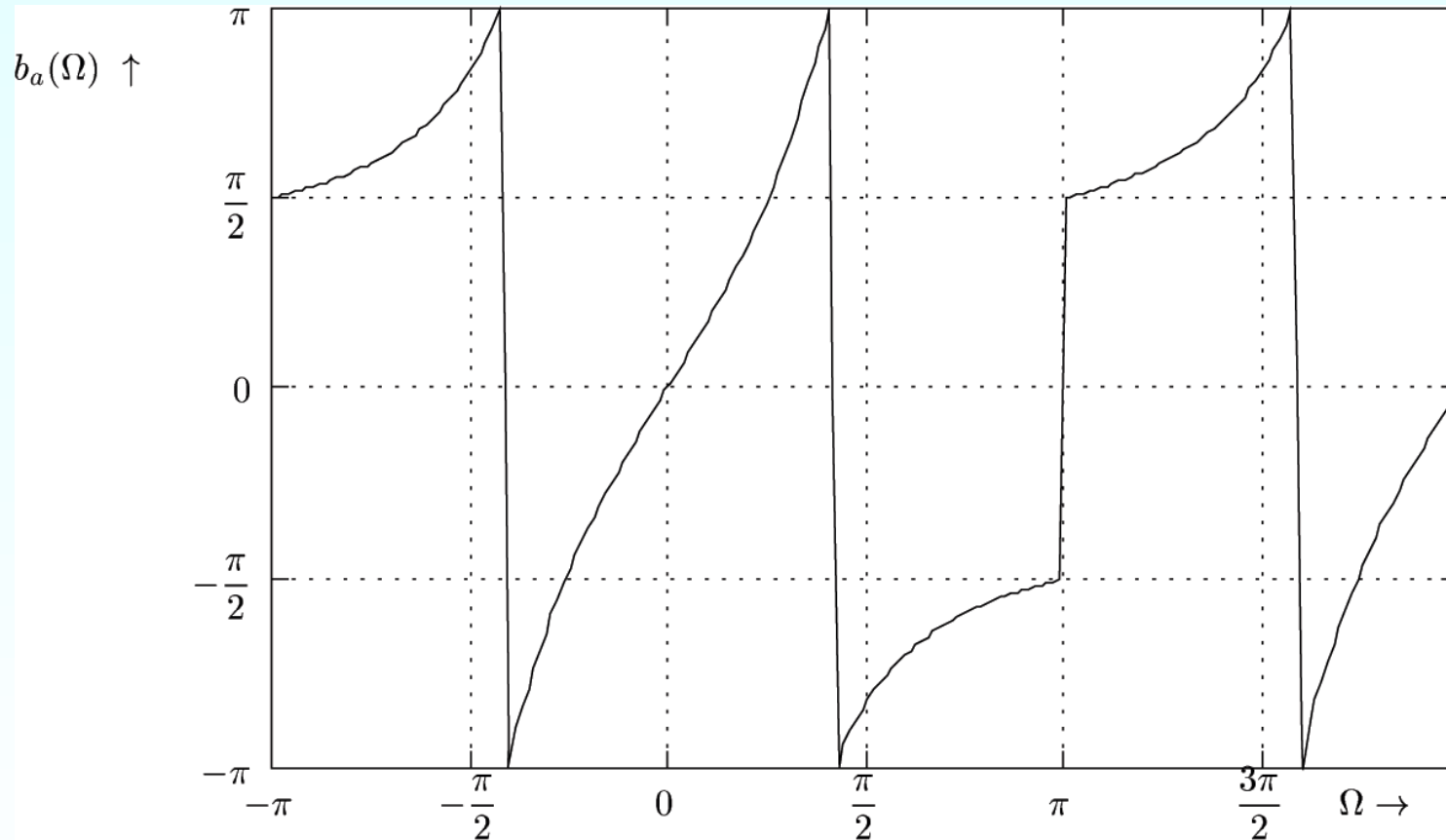
Example: 3rd order system with the discrete transfer function

$$H(z) = \frac{(z+1)(z+0.2)}{(z-0.3)(z-0.3-j0.6)(z-0.3+j0.6)}$$



Magnitude of discrete transfer function of 3rd order system

4.2.5 Behaviour of $H_z(z)$ on the unit circle



Phase of discrete transfer function of 3rd order system

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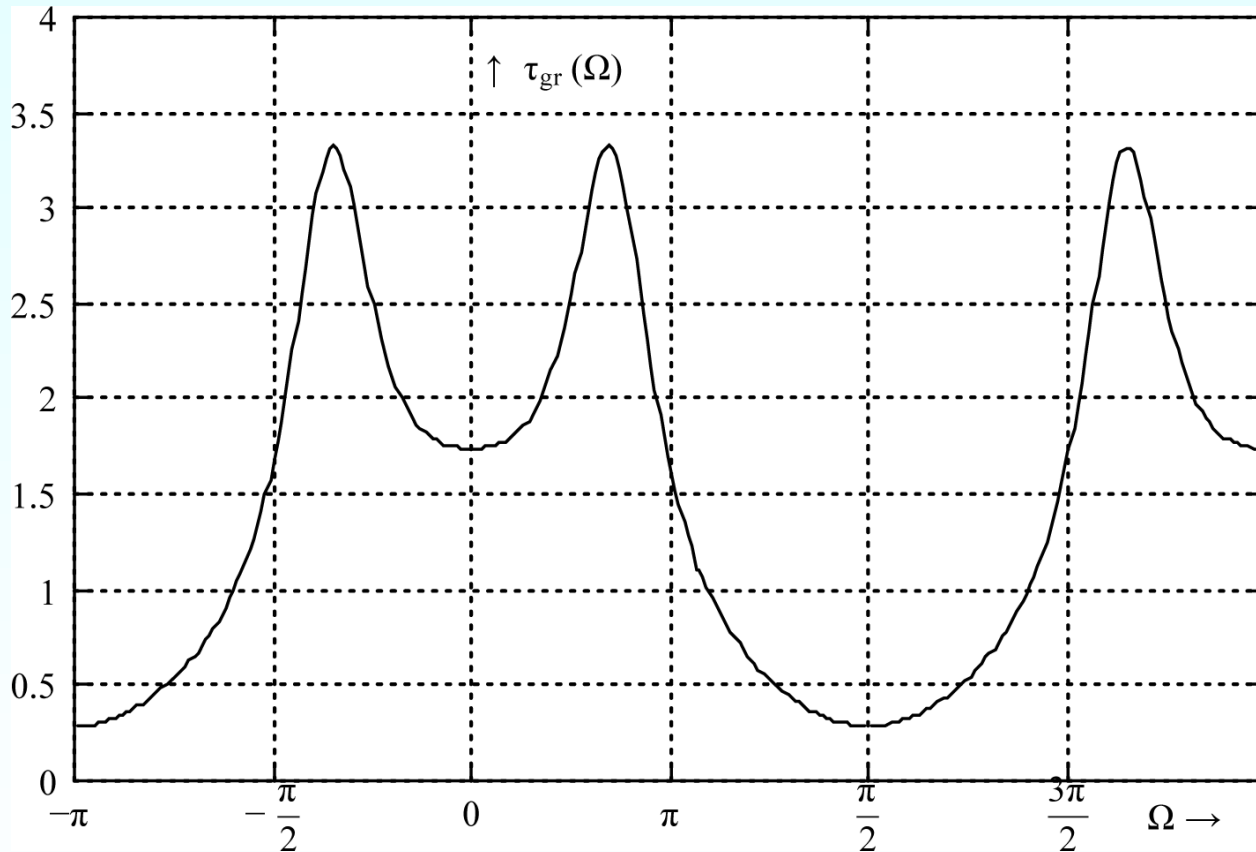
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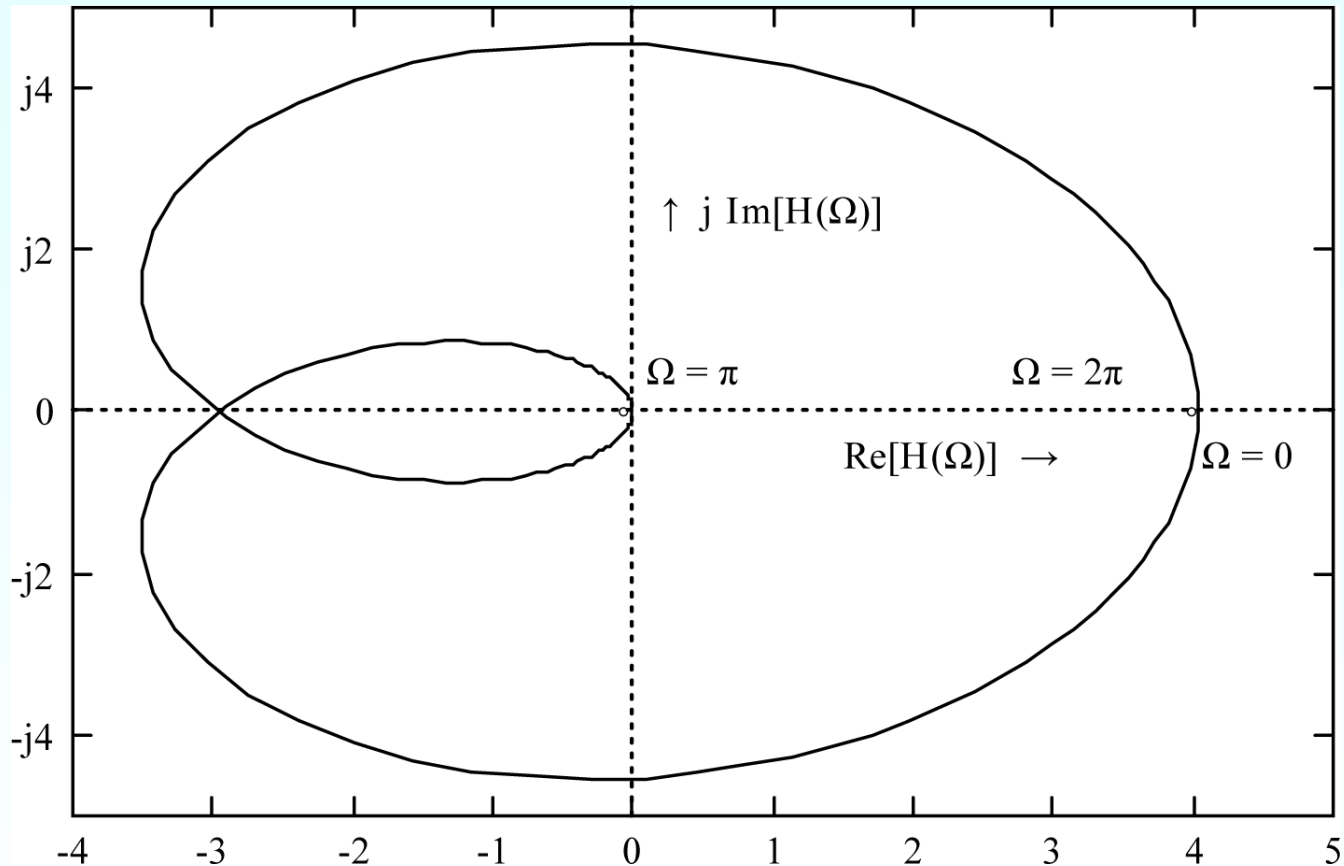


4.2.5 Behaviour of $H_z(z)$ on the unit circle



Envelope delay of a 3rd order system

4.2.5 Behaviour of $H_z(z)$ on the unit circle



Locus of the discrete transfer function of 3rd order system

4.2.5 Behaviour of $H_z(z)$ on the unit circle

If the regarded system are causal and stable then:

1. $H_L(p)$ is analytically regular for $\text{Re } p > 0$ and $H_z(z)$ is analytically regular for $|z| < 1$
2. $H_L(j\omega) = H(\omega)$ shows the frequency behaviour of analog filter
 $H_z(e^{j\omega T}) = H_z(e^{j\Omega}) = H_a(\omega)$ shows the frequency behaviour of digital filter.

with
$$H_z(e^{j\Omega}) = \text{Re}\{H_z(e^{j\Omega})\} + j \text{Im}\{H_z(e^{j\Omega})\} \quad \text{or}$$

$$H_{Na}(\Omega) = \text{Re}\{H_{Na}(\Omega)\} + j \text{Im}\{H_{Na}(\Omega)\}$$

It results:

$$\text{Re}\{H_{Na}(\Omega)\} = \lim_{z \rightarrow \infty} H_z(z) - \frac{1}{2\pi} \int_{-\pi}^{+\pi} \text{Im}\{H_{Na}(\eta)\} \cot \frac{\eta - \Omega}{2} d\eta$$

$$\text{Im}\{H_{Na}(\Omega)\} = \frac{1}{2\pi} \int_{-\pi}^{+\pi} \text{Re}\{H_{Na}(\eta)\} \cot \frac{\eta - \Omega}{2} d\eta$$



4.2.5 Behaviour of $H_z(z)$ on the unit circle

Note: For minimum-phase systems, it applies:

$$\ln |H_{Na}(\Omega)| = \lim_{z \rightarrow \infty} \ln |H_z(z)| - \frac{1}{2\pi} \int_{-\pi}^{+\pi} \varphi_a(\eta) \cot \frac{\eta - \Omega}{2} d\eta$$

$$\varphi_{Na}(\Omega) = \frac{1}{2\pi} \int_{-\pi}^{+\pi} \ln |H_{Na}(\eta)| \cot \frac{\eta - \Omega}{2} d\eta$$



4.2.6 All-Pass Filters

An all-pass filter is defined according to:

$$|H_a(\Omega)| = |H_z(e^{j\Omega})| = \text{const. } \forall \Omega$$

For the discrete transfer function of an all-pass: $H_z(z) = \frac{P(z)}{Q(z)}$

one observes:

$$\frac{1}{Q(z)} = \frac{1}{c_n \prod_{\nu=1}^n (z - z_{\infty\nu})}$$

and looks for a:

$$P(z) = b_m \prod_{\mu=1}^m (z - z_{0\mu})$$

In such a way that equation is fulfilled.



4.2.6 All-Pass Filters

The following possibilities are given:

□ Case $z_{\infty\nu} = 0$, $\forall \nu$

$$|H_{Na}(\Omega)| = \frac{1}{|c_n|} \text{ where } P(z) = 1, \text{ because } |z| = 1 \text{ where } z = e^{j\Omega}$$

• Other case it results:

$$|H_{Na}(\Omega)| = \left| \frac{d_m}{c_n} \frac{\prod_{\mu=1}^m \sqrt{1 - 2|z_{0\mu}| \cos(\Omega - \psi_{0\mu}) + |z_{0\mu}|^2}}{\prod_{\nu=1}^n \sqrt{1 - 2|z_{\infty\nu}| \cos(\Omega - \psi_{\infty\nu}) + |z_{\infty\nu}|^2}} \right|$$

So every pole makes a contribution $\sqrt{1 - 2|z_{\infty\nu}| \cos(\Omega - \psi_{\infty\nu}) + |z_{\infty\nu}|^2}$ to $|H_{Na}(\Omega)|$



4.2.6 All-Pass Filters

$|H_{Na}(\Omega)| = \text{const.}$ results in case the contribution of every pole is compensated by :

$$\sqrt{1 - 2|z_{0\mu}|\cos(\Omega - \psi_{0\mu}) + |z_{0\mu}|^2}$$

This is possible, if $m=n$ and:

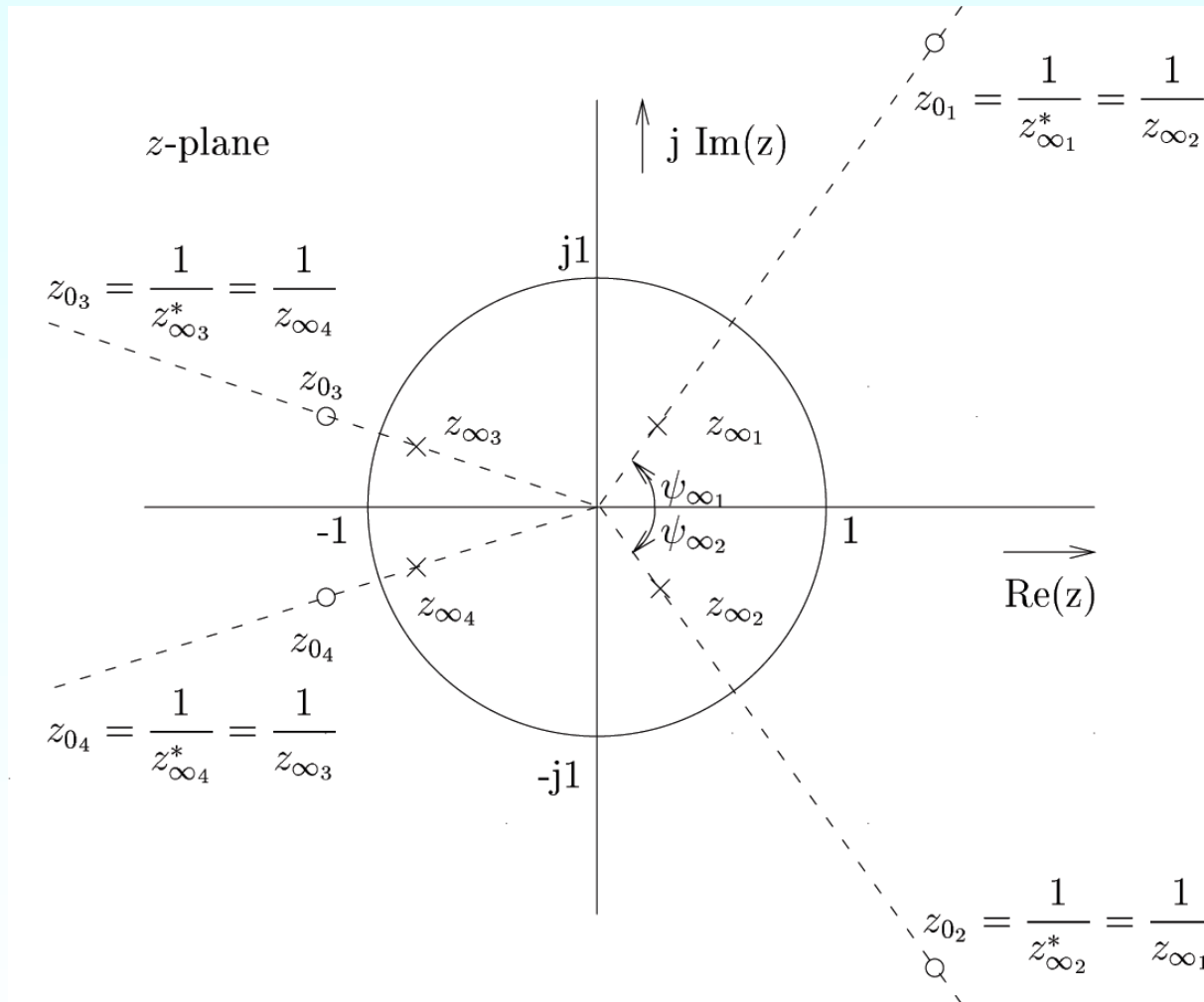
$$z_{0\mu} = |z_{0\mu}| e^{j\psi_{0\mu}} = \frac{1}{|z_{\infty\nu}|} e^{j\psi_{\infty\nu}} = \frac{1}{|z_{\infty\nu}| e^{-j\psi_{\infty\nu}}} = \frac{1}{z_{\infty\nu}^*}$$

so that:

$$\frac{|e^{j\Omega} - z_{0\mu}|}{|e^{j\Omega} - z_{\infty\nu}|} = \frac{\sqrt{1 - 2\frac{1}{|z_{\infty\nu}|}\cos(\Omega - \Psi_{\infty\nu}) + \frac{1}{|z_{\infty\nu}|^2}}}{\sqrt{1 - |z_{\infty\nu}|\cos(\Omega - \Psi_{\infty\nu}) + |z_{\infty\nu}|^2}} = \frac{1}{|z_{\infty\nu}|}$$



4.2.6 All-Pass Filters



Pole-Zero diagram of an All-pass in the z-plane

4.2.6 All-Pass Filters

One gets in case of:

$$|z_{\infty\nu}| = \frac{1}{|z_{0\nu}|} \quad \text{and} \quad \Psi_{\infty\nu} = \Psi_{0\nu}$$

phase delay:

$$\varphi_{Na}(\Omega) = \sum_{\nu=1}^n \arctan \frac{(1 - |z_{\infty\nu}|^2) \sin(\Omega - \Psi_{\infty\nu})}{(1 + |z_{\infty\nu}|^2) \cos(\Omega - \Psi_{\infty\nu}) - 2|z_{\infty\nu}|}$$

envelope delay:

$$\tau_{Nga}(\Omega) = \sum_{\nu=1}^n \frac{1 - |z_{\infty\nu}|^2}{1 - 2|z_{\infty\nu}| \cos(\Omega - \Psi_{\infty\nu}) + |z_{\infty\nu}|^2} \quad \text{where} \quad |z_{\infty\nu}| < 1 \quad \text{for all } \nu$$



4.2.7 Minimum-phase Systems

Discrete system can also be divided into all-passes and minimum-phase systems

Let's assume an stable LTI discrete system with the transfer function:

$$H_z(z) = \frac{d_m \prod_{\mu=1}^m (z - z_{0\mu})}{c_n \prod_{\nu=1}^n (z - z_{\infty\nu})} = \frac{d_m \prod_{\mu=1}^{m_1} (z - z_{0\mu}^{(1)})}{c_n \prod_{\nu=1}^n (z - z_{\infty\nu})} \prod_{\mu=m_1+1}^m (z - z_{0\mu}^{(2)})$$

with $|z_{0\mu}^{(1)}| \leq 1$ for $\mu = 1, \dots, m_1$ the first m_1 zeros in the unit-circle

$|z_{0\mu}^{(2)}| > 1$ for $\mu = m_1 + 1, \dots, m$ other zeros outside the unit-circle



4.2.7 Minimum-phase Systems

With $\prod_{\mu=m_1+1}^m (z^{(2)}_{0\mu} \cdot z - 1) = \prod_{\mu=m_1+1}^m z^{(2)}_{0\mu} (z - \frac{1}{z^{(2)}_{0\mu}})$, it yields:

$$H_z(z) = \frac{b_m \prod_{\mu=1}^{m_1} (z - z^{(1)}_{0\mu}) \prod_{\mu=m_1+1}^m (z^{(2)}_{0\mu} \cdot z - 1)}{c_n \underbrace{\prod_{v=1}^n (z - z_{\infty v})}_{H_{z_M}(z)}} \cdot \frac{\prod_{\mu=m_1+1}^m (z - z^{(2)}_{0\mu})}{\underbrace{\prod_{\mu=m_1+1}^m z^{(2)}_{0\mu} (z - \frac{1}{z^{(2)}_{0\mu}})}_{H_{z_{Allp.}}}}$$

Or in a short form:

$$H_z(z) = H_{z_M}(z) \cdot H_{z_{Allp.}}(z)$$



4.2.7 Minimum-phase Systems

With $z_{0\mu}^{(2)} = \frac{1}{z_{\infty\mu}}$, one obtains for the all-pass:

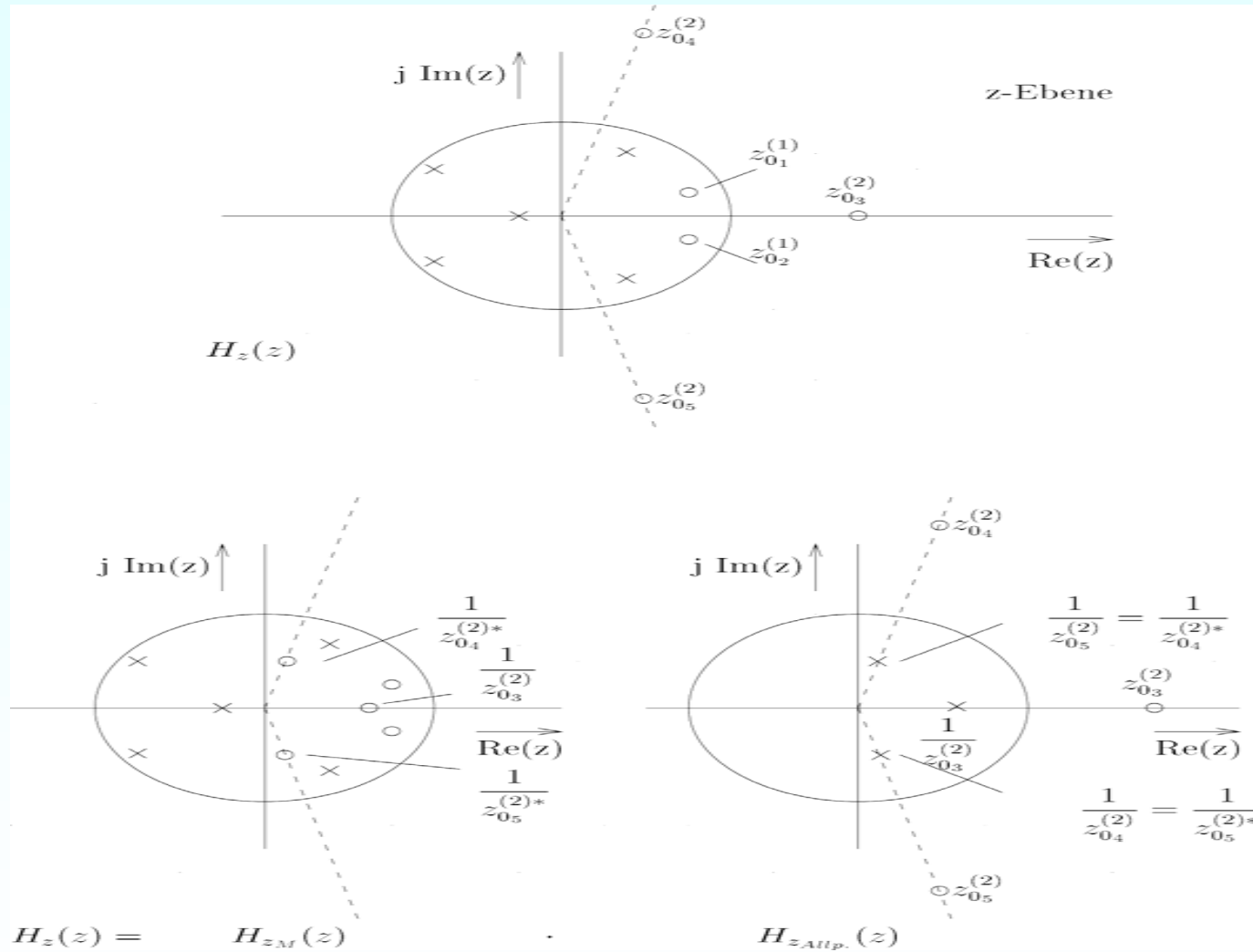
$$H_{z_{Allp.}}(z) = \frac{1}{\underbrace{\prod_{\mu=m_1+1}^m z_{0\mu}^{(2)}}_{\text{real constant}}} \cdot \frac{\prod_{\mu=m_1+1}^m (z - \frac{1}{z_{\infty\mu}})}{\prod_{\mu=m_1+1}^m (z - z_{\infty\mu})}$$

$$\text{Because } |z_{0\mu}^{(2)}| > 1 \Leftrightarrow |z_{\infty\mu}| = \frac{1}{|z_{0\mu}^{(2)}|} < 1$$

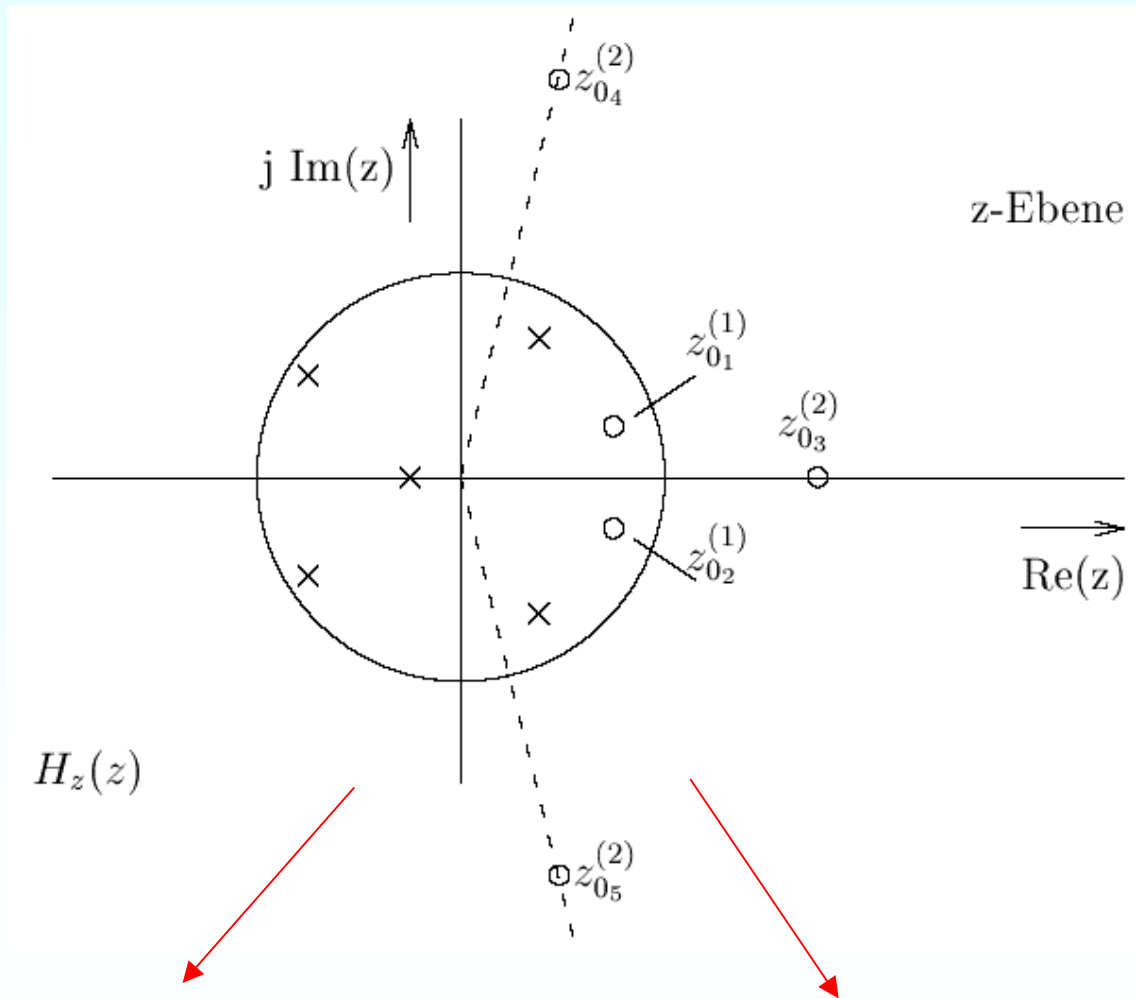
The poles of this all-pass lie inside the unit-circle



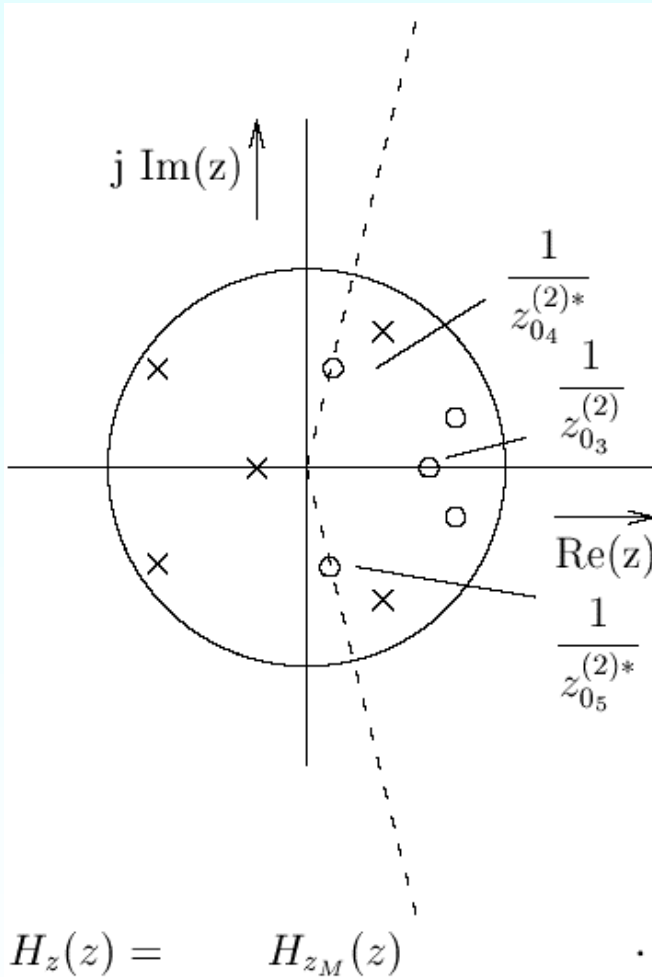
4.2.7 Minimum-phase Systems



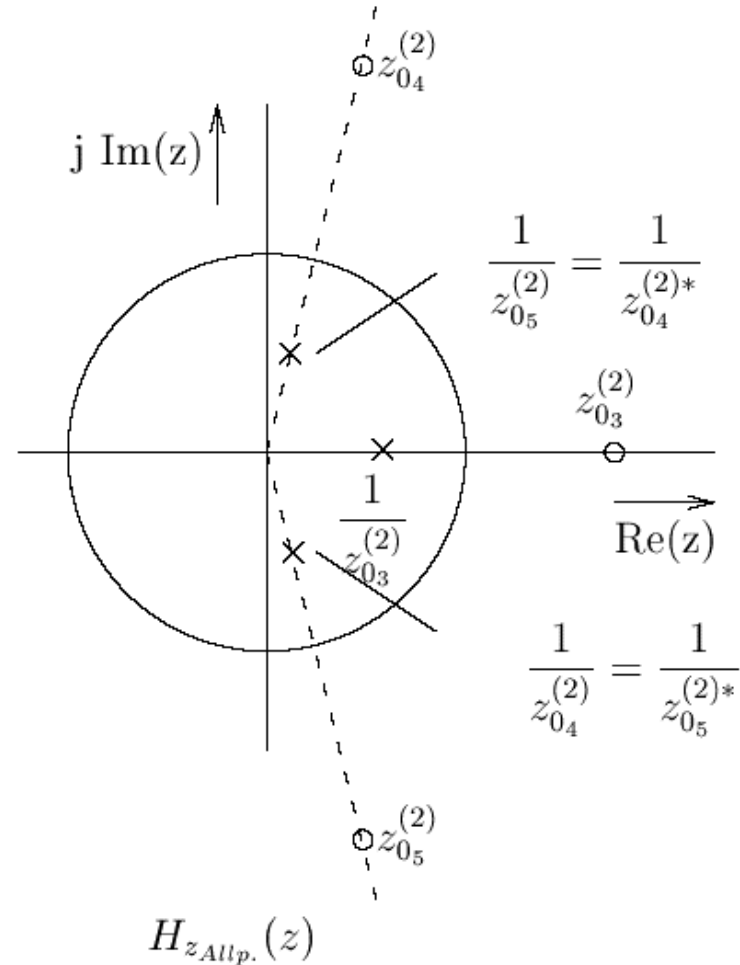
4.2.7 Minimum-phase Systems



4.2.7 Minimum-phase Systems



Minimum phase system



All pass system

4.2.8 Systems with Linear Phase

Linear phase means a constant envelope delay with the frequency

$$\tau_{Nga}(\Omega) \neq f(\Omega)$$

where:

$$\tau_{Nga}(\Omega) = \sum_{\nu=1}^n \frac{1 - |z_{\infty\nu}| \cos(\Omega - \Psi_{\infty\nu})}{1 - 2|z_{\infty\nu}| \cos(\Omega - \Psi_{\infty\nu}) + |z_{\infty\nu}|^2} - \sum_{\mu=1}^m \frac{1 - |z_{0\mu}| \cos(\Omega - \Psi_{0\mu})}{1 - 2|z_{0\mu}| \cos(\Omega - \Psi_{0\mu}) + |z_{0\mu}|^2}$$

The condition is fulfilled in cases:

1. $n = m$ and $z_{0\mu} = z_{\infty\nu}$ for all $\nu = \mu \Rightarrow$ **poles and zeros exhibit the same location**
2. $|z_{0\mu}| = 1 \quad \forall \mu$ **and** $|z_{\infty\nu}| = 1 \quad \forall \nu \Rightarrow$ leads to only conditional stable systems and therefore is ignored in the following:



4.2.8 Systems with Linear Phase

A) $|z_{\infty\nu}| < 1 \quad \forall \nu$ must be fulfilled, $|z_{\infty\nu}| = 0 \quad \forall \nu$ ensures that a frequency independent contribution from the poles is introduced in the formula for the group delay.

B) The zeros $z_{0\mu}$ have to be located in such a way, that:

$$\sum_{\mu=1}^m \frac{1 - |z_{0\mu}| \cos(\Omega - \Psi_{0\mu})}{1 - 2|z_{0\mu}| \cos(\Omega - \Psi_{0\mu}) + |z_{0\mu}|^2} \rightarrow \text{const.}$$

To fulfill B) condition, it is required:

$$1) \quad H_z(z) = \frac{b_m \prod_{\mu=1}^m (z - z_{0\mu})}{c_n \prod_{\nu=1}^n (z - z_{\infty\nu})} = \frac{b_m}{c_n} \frac{1}{z^n} \prod_{\mu=1}^m (z - z_{0\mu}) \Rightarrow \text{non-recursive system.}$$



4.2.8 Systems with Linear Phase

2) The zeros $z_{0\mu}$ have to be located pair-wise symmetrically to each other:

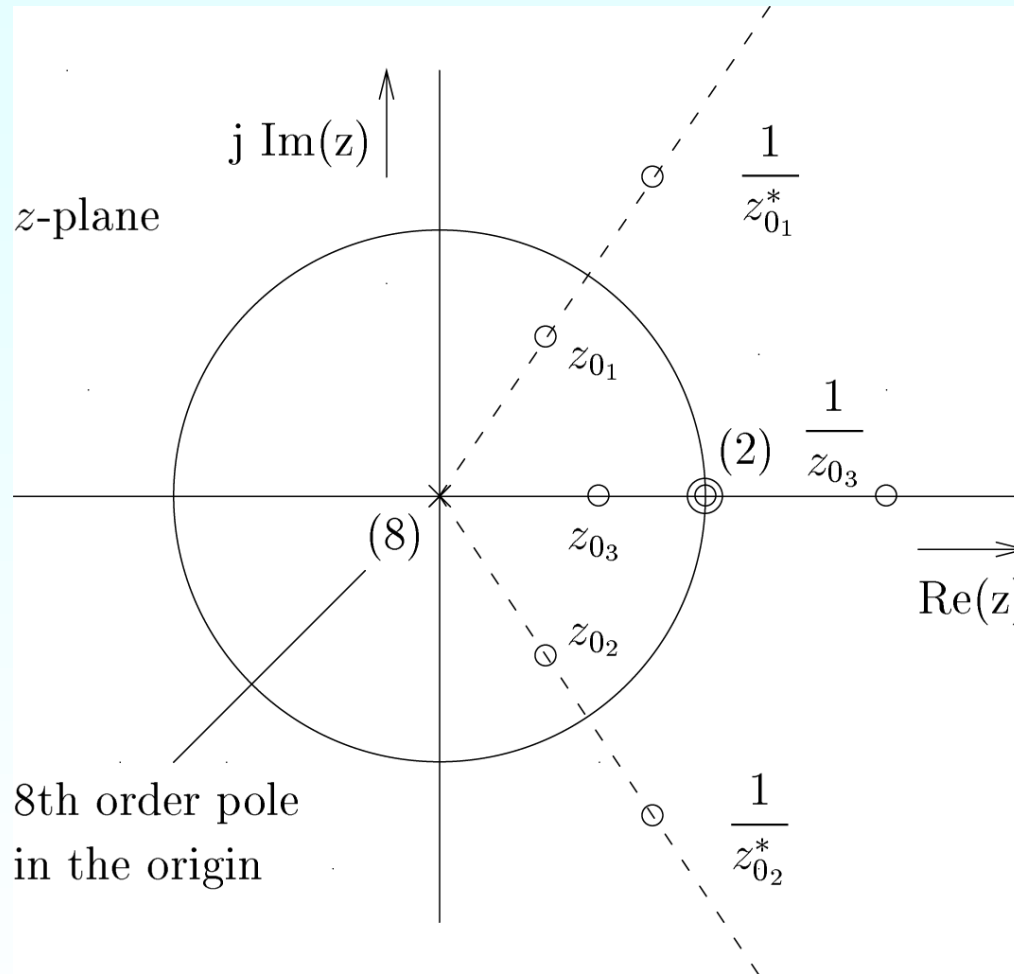
$$z_{0_a} = |z_{0_a}| e^{j\Psi_{0_a}} = \frac{1}{z_{0_b}^*} = \left| \frac{1}{z_{0_b}} \right| e^{j\Psi_{0_b}}$$

Due to this relation, the total group delay gives:

$$\begin{aligned} & \frac{1 - |z_{0_a}| \cos(\Omega - \Psi_{0_a})}{1 - 2|z_{0_a}| \cos(\Omega - \Psi_{0_a}) + |z_{0_a}|^2} + \frac{1 - |z_{0_b}| \cos(\Omega - \Psi_{0_b})}{1 - 2|z_{0_b}| \cos(\Omega - \Psi_{0_b}) + |z_{0_b}|^2} \\ &= \frac{1 - |z_{0_a}| \cos(\Omega - \Psi_{0_a})}{1 - 2|z_{0_a}| \cos(\Omega - \Psi_{0_a}) + |z_{0_a}|^2} + \frac{1 - \frac{1}{|z_{0_a}|} \cos(\Omega - \Psi_{0_a})}{1 - \frac{2}{|z_{0_a}|} \cos(\Omega - \Psi_{0_a}) + \frac{1}{|z_{0_a}|^2}} = 1 \end{aligned}$$



4.2.8 Systems with Linear Phase



Pole-Zero diagram of Non-Recursive System with Linear Phase

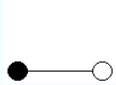
4.2.8 Systems with Linear Phase

Therefore discrete systems with linear phase have always a transfer function :

$$H_z(z) = \frac{b_m}{c_n} \frac{1}{z^n} (z-1)^{m_3} (z+1)^{m_2} \prod_{\mu=1}^{m_1} (z - z_{0\mu}) \left(z - \frac{1}{z_{0\mu}^*}\right)$$

where $2m_1 + m_2 + m_3 = m \leq n$

Example: for $n=1 \Rightarrow m=0$, i.e., $m_1 = m_2 = m_3 = 0$

and $H_z(z) = \frac{b_m}{c_n} z^{-1}$  $h(k) = \frac{b_m}{c_n} \gamma_0(k-1)$



Delay element with $\frac{b_m}{c_n} = 1$

4.2.9 Non-Recursive Systems (FIR-Filters)

Non-recursive systems have been defined by:

$$g(k) = \frac{1}{b_0} \sum_{\alpha=\varepsilon}^n a_\alpha s(k - \alpha) \quad \text{○} \text{---} \text{●} \quad G(z) = \frac{1}{b_0} \sum_{\alpha=\varepsilon}^n a_\alpha S(z) z^{-\alpha}$$

or

$$H_z(z) = \frac{G(z)}{S(z)} = \frac{1}{b_0} \sum_{\alpha=0}^n a_\alpha z^{-\alpha}$$

Properties:

1. Because of $H_z(z) = \sum_{v=0}^m h(v) z^{-v}$, the impulse response:

$$h(k) = \frac{a_k}{b_0} \quad \text{for } k = 0 \dots n \quad \text{with } h(k) = 0 \quad \text{for } k < 0 \quad \text{and } k > n$$

finite duration \Rightarrow also called FIR (Finite Impulse Response) - systems.

With the output signal: $g(k) = s(k) * h(k) = \sum_{v=0}^n h(v) s(k - v)$



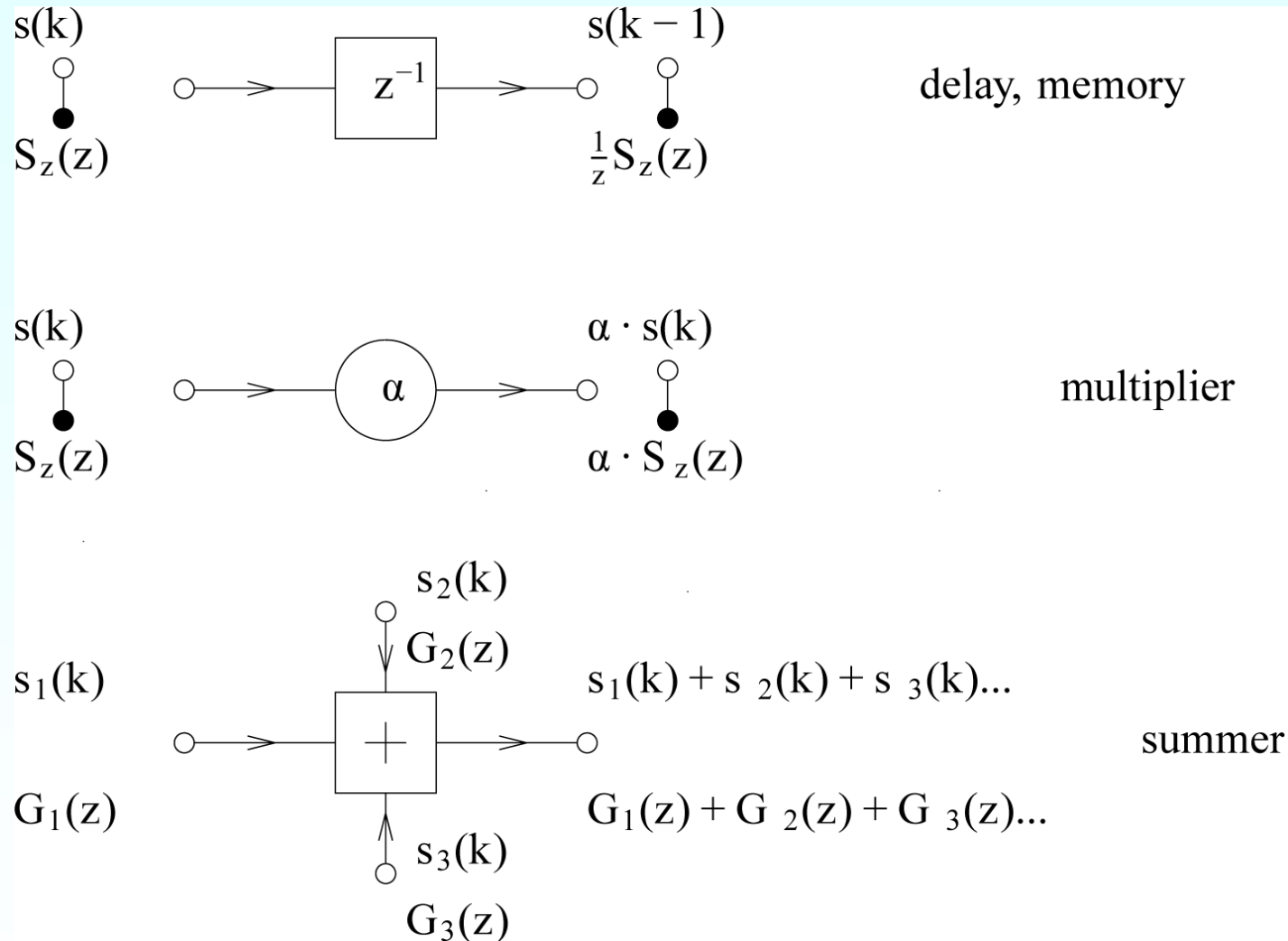
4.2.9 Non-Recursive Systems (FIR-Filters)

2. From this results:
$$H_z(z) = \frac{1}{b_0} \sum_{\alpha=0}^n a_{\alpha} z^{-\alpha} = \frac{1}{b_0} \sum_{\alpha=0}^n \frac{a_{\alpha} z^{n-\alpha}}{z^n}$$

non-recursive systems have just an nth order pole at $z = 0 \rightarrow$ always stable!



4.3 System Structures for Discrete LTI-Systems



4.3.1 The First Canonical Form of a Discrete System

A canonical form is a system structure with a minimized number of memories (delay elements).

From chapter 4.2.1:
$$g(k) = \frac{1}{b_0} \left[\sum_{\alpha=0}^n a_{\alpha} s(k - \alpha) - \sum_{\beta=1}^n b_{\beta} g(k - \beta) \right]$$

by setting $m = n$ one obtains:

$$g(k) = \frac{1}{b_0} \left[\sum_{\alpha=0}^n a_{\alpha} s(k - \alpha) - \sum_{\beta=1}^n b_{\beta} g(k - \beta) \right]$$

or

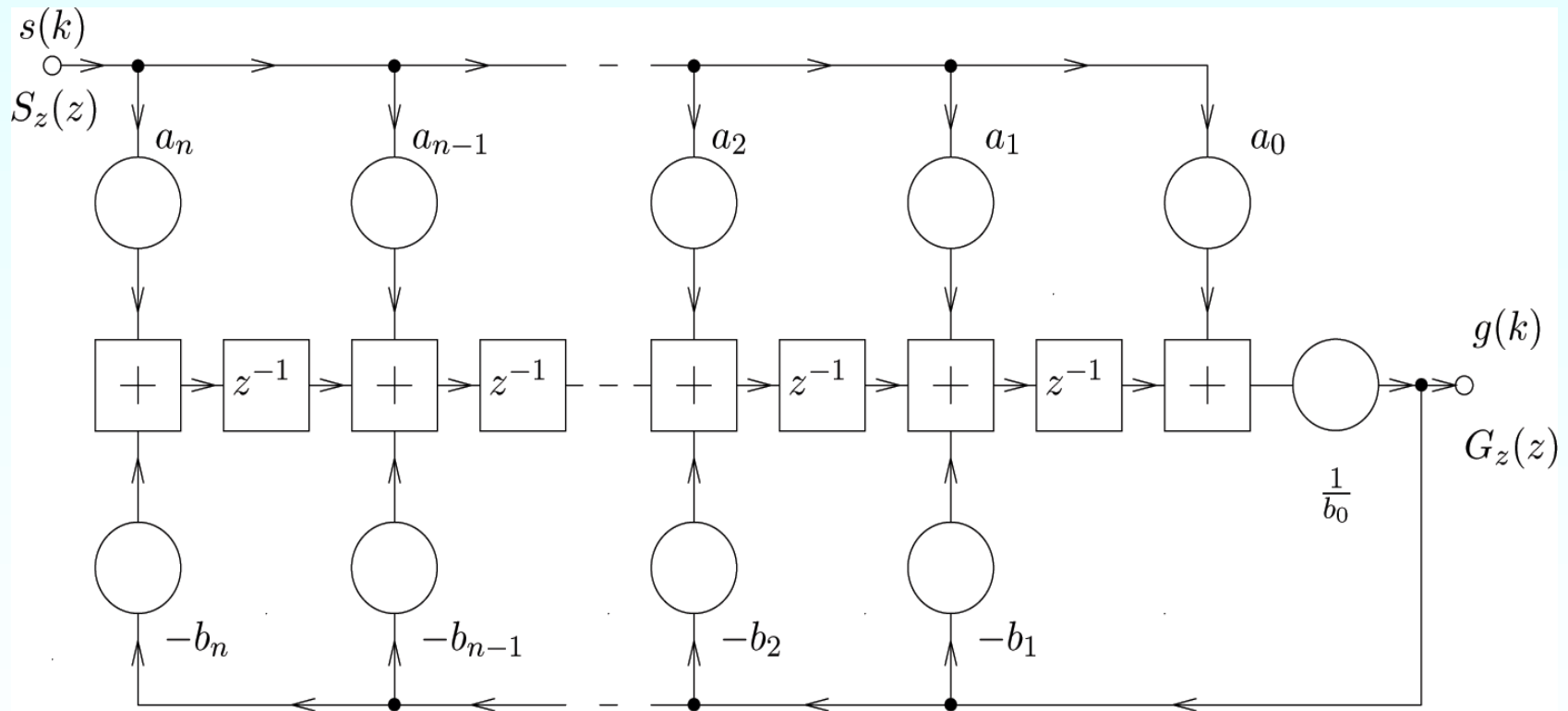
$$g(k) = \frac{a_0}{b_0} s(k) + \frac{1}{b_0} \left[\sum_{\gamma=1}^n \{ a_{\gamma} s(k - \gamma) - b_{\gamma} g(k - \gamma) \} \right]$$

○
|
●

$$G_z(z) = \frac{a_0}{b_0} S_z(z) + \frac{1}{b_0} \left[\sum_{\gamma=1}^n \{ a_{\gamma} S_z(z) z^{-\gamma} - b_{\gamma} G_z(z) z^{-\gamma} \} \right]$$



4.3.1 The First Canonical Form of a Discrete System



First Canonical form of a digital filter

4.3.2 The Second Canonical Form of a Discrete Filter

A second canonical form results as follows:

$$G_z(z) = \frac{\sum_{\mu=0}^n d_{\mu} z^{\mu}}{\sum_{\nu=0}^n c_{\nu} z^{\nu}} S_z(z)$$

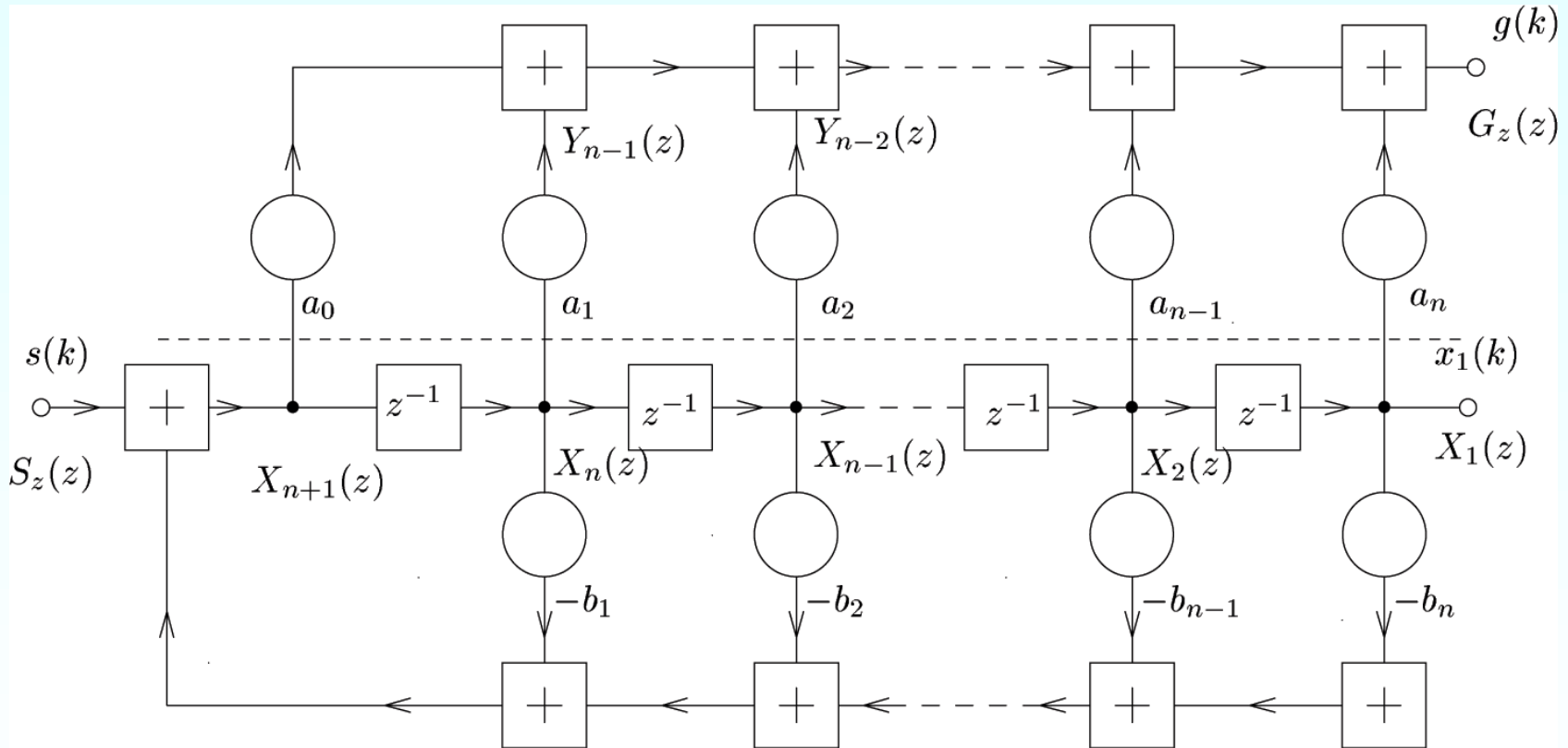
The second form works equal to the first canonical form; this is proved in the following:

- The representation in following figure with

$$H_z(z) = \frac{G_z(z)}{S_z(z)} = \frac{\sum_{\mu=0}^n b_{\mu} z^{\mu}}{\sum_{\nu=0}^n c_{\nu} z^{\nu}} \quad \text{equals the one in figure of the 1st Form}$$



4.3.2 The Second Canonical Form of a Discrete Filter



The Second Canonical Form of a Digital Filter

4.3.2 The Second Canonical Form of a Discrete Filter

First, one takes a look at the part underneath the dashed line → this system part can obviously be described by:

$$s(k) \rightarrow x_1(k) \quad \text{---} \bullet \quad S_z(z) \rightarrow X_1(z)$$

Furthermore:

$$X_1(z) = z^{-n} X_{n+1}(z) \xrightarrow{\text{in general}} X_{\nu+1}(z) = z^{\nu} X_1(z)$$

Due to $x_{n+1}(k) = s(k) - \sum_{\nu=1}^n b_{\nu} x_{n-\nu+1}(k)$, we obtain:

$$\begin{aligned} X_{n+1}(z) = S_z(z) - \sum_{\nu=1}^n b_{\nu} X_{n-\nu+1}(z) &\Leftrightarrow z^n X_1(z) = S_z(z) - \sum_{\nu=1}^n b_{\nu} X_{n-\nu+1}(z) \\ &= S_z(z) - \sum_{\nu=1}^n b_{\nu} z^{n-\nu} X_1(z) \end{aligned}$$



4.3.2 The Second Canonical Form of a Discrete Filter

$$\Leftrightarrow X_1(z) \left[z^n + z^n \sum_{\nu=1}^{n-1} b_\nu z^{-\nu} \right] = S_z(z)$$

and with $b_0 = 1$ we obtain:
$$X_1(z) = \frac{S_z(z)}{z^n \sum_{\nu=0}^n b_\nu z^{-\nu}}$$

For the upper part of the system the difference equation $g(k) = \sum_{\nu=0}^n a_\nu x_{n-\nu+1}(k)$ results:

$$\begin{aligned} G_z(z) &= \sum_{\nu=0}^n a_\nu X_{n-\nu+1}(z) = \sum_{\nu=0}^n a_\nu z^{n-\nu} X_1(z) \\ &= X_1(z) z^n \sum_{\nu=0}^n a_\nu z^{-\nu} = \frac{z^n \sum_{\nu=0}^n a_\nu z^{n-\nu}}{z^n \sum_{\nu=0}^n b_\nu z^{-\nu}} S_z(z) \end{aligned}$$



4.3.2 The Second Canonical Form of a Discrete Filter

or:

$$G_z(z) = \frac{\sum_{v=0}^n a_v z^{-v}}{\sum_{v=0}^n b_v z^{-v}} S_z(z)$$

So the whole system is described by:

$$H_z(z) = \frac{G_z(z)}{S_z(z)} = \frac{\sum_{v=0}^n a_v z^{-v}}{\sum_{v=0}^n b_v z^{-v}}$$



4.3.3 The Third Canonical Form of a Digital System

3rd Form: cascade of the 1st and 2nd order system.

One can divide from:

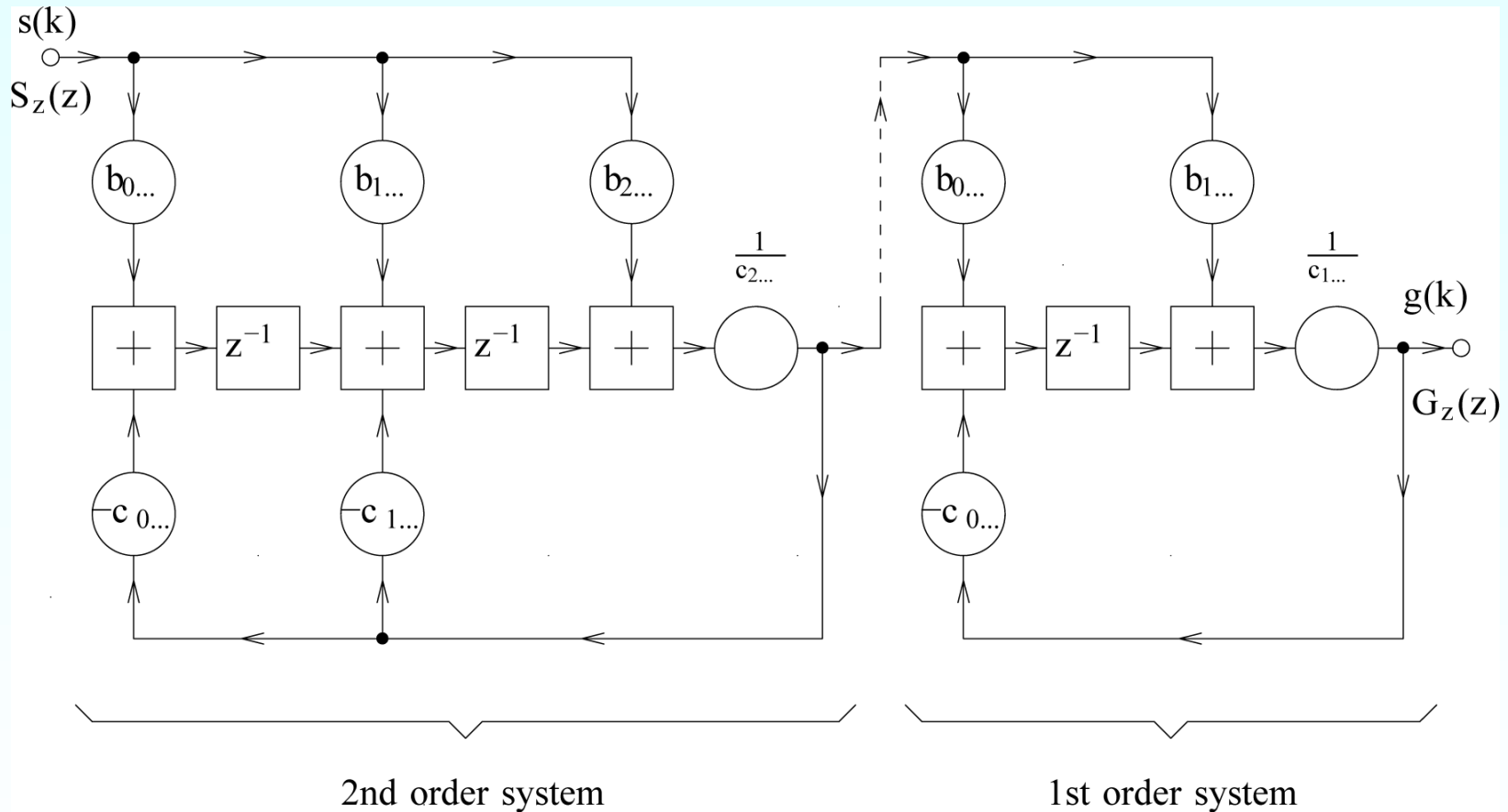
$$H_z(z) = \frac{d_m \prod_{\mu=1}^m (z - z_{0\mu})}{c_n \prod_{\nu=0}^n (z - z_{\infty\nu})} = \prod_{\gamma=1}^{\dots} H_{z\gamma}(z)$$

into

$$H_{z\gamma}(z) = \frac{d_{1\gamma} z + d_{0\gamma}}{c_{1\gamma} z + c_{0\gamma}} \quad \text{and} \quad H_{z\gamma}(z) = \frac{d_{2\gamma} z^2 + d_{1\gamma} z + d_{0\gamma}}{c_{2\gamma} z^2 + c_{1\gamma} z + c_{0\gamma}}$$



4.3.4 The Fourth Canonical form of a Digital Filter



Cascade of a 1st and 2nd Order Digital Filter

4.3.4 The Fourth Canonical form of a Digital Filter

Another canonical structure can be obtained by converting the transfer function into a partial sum:

$$H_z(z) = \frac{\sum_{\mu=0}^m d_{\mu} z^{\mu}}{c_n \prod_{v=1}^n (z - z_{\infty v})} = R_{\infty} + \sum_{v=1}^n \frac{R_v}{(z - z_{\infty v})}$$

The residues in this simple case follow from (where $c_n = 1$):

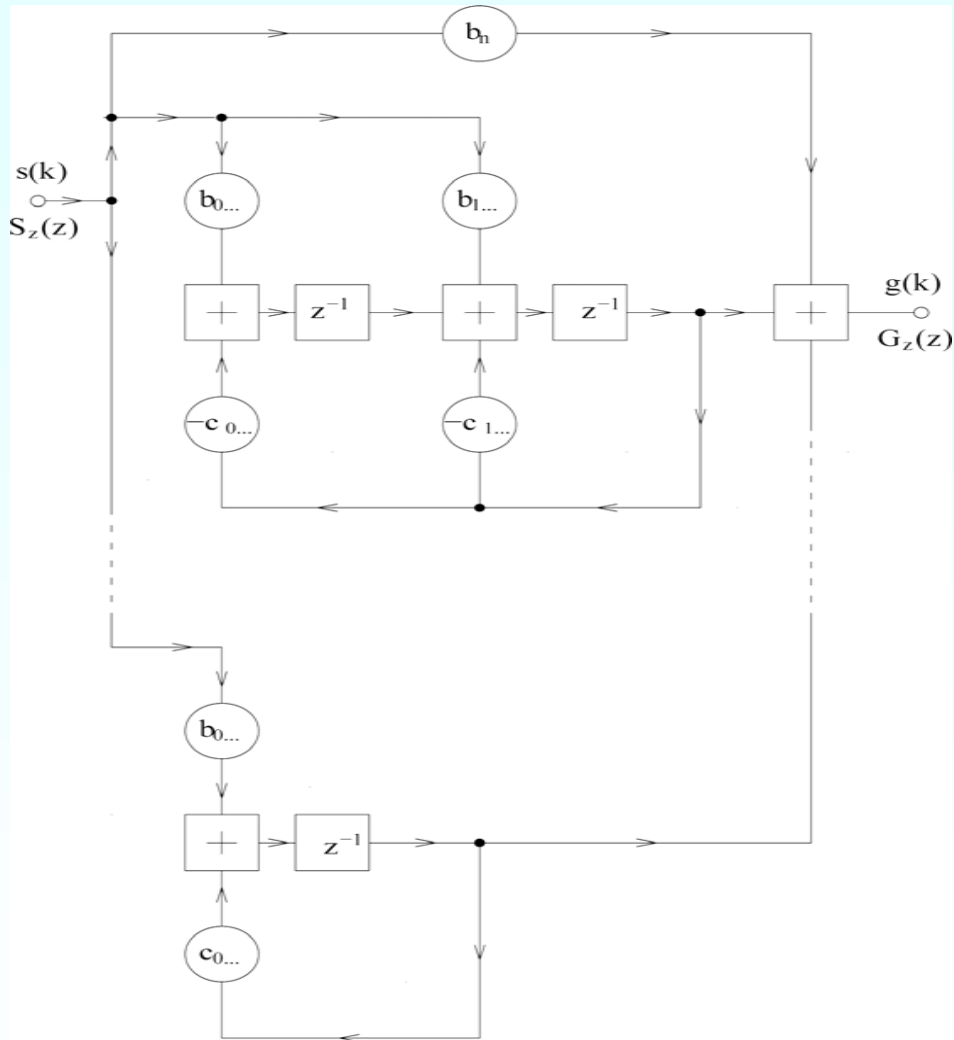
$$R_{\infty} = \lim_{z \rightarrow \infty} H_z(z) = d_n \quad \text{for } m = n$$

$$R_v = \lim_{z \rightarrow z_{\infty v}} \{(z - z_{\infty v}) H_z(z)\} \quad \text{for single poles}$$

➡ **This leads to a parallel connection of the parts.**



4.3.4 The Fourth Canonical form of a Digital Filter



4.3.4 The Fourth Canonical form of a Digital Filter

For real poles: $H_{z\gamma}(z) = \frac{d_{0\gamma}}{z + c_{0\gamma}}$ where $d_{0\gamma} = R_\gamma$ and $c_{0\gamma} = -z_{\infty\gamma}$

For conjugate complex poles, two terms must be combined:

$$H_{z\gamma}(z) = \frac{b_{1\gamma} z + b_{0\gamma}}{z^2 + c_{1\gamma} z + c_{0\gamma}} \quad \text{where}$$

$$d_{0\gamma} = -2 \operatorname{Re} \{ R_\gamma z_{\infty\gamma}^* \}, \quad d_{1\gamma} = 2 \operatorname{Re} \{ R_\gamma \}, \quad c_{0\gamma} = |z_{\infty\gamma}|^2 \quad \text{and} \quad c_{1\gamma} = -2 \operatorname{Re} \{ z_{\infty\gamma} \}$$

So in completion:

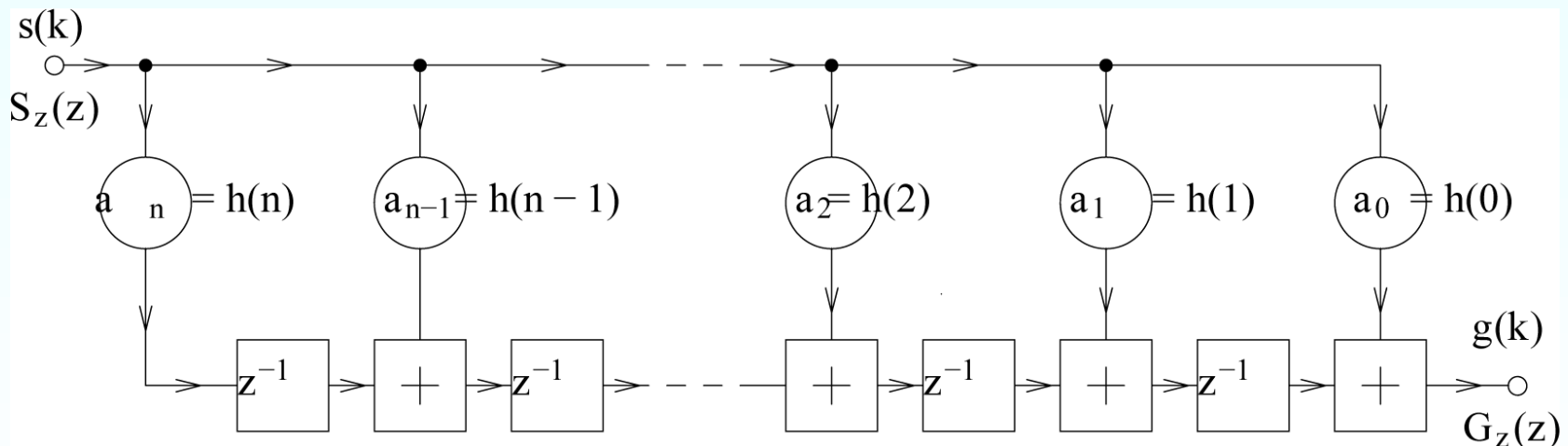
$$H_z(z) = d_n + \sum_{\gamma=1}^{\dots} H_{z\gamma}(z) \quad \text{where} \quad c_n = 1$$



4.3.5 System Structures for Non-Recursive Systems (FIR-Filters)

For any of the first three canonical forms, an appropriate non-recursive system can be directly derived from equation

$$g(k) = \frac{1}{b_0} \sum_{\alpha=0}^n a_{\alpha} s(k - \alpha)$$



First Canonical Form of a FIR - Filter